



IN THE U.S. PATENT AND TRADEMARK OFFICE

Applicant:

KANAMARU et al.

Conf.: UNASSIGNED

Appl. No.:

10/815,790

Group: UNASSIGNED

Filed:

April 2, 2004 Examiner: UNASSIGNED

For:

TONER FOR DEVELOPMENT OF ELECTROSTATIC

LATENT IMAGES

LETTER SUBMITTING 37 CFR § 1.132 DECLARATION

MAY 1 1 2004

Commissioner for Patents P.O. Box 1450 Alexandria, VA 22313-1450

REMARKS

Attached hereto is a Declaration under 37 CFR § 1.132 by Mr. Yutaka Kanamaru, one of the co-inventors of the above-identified application. The USPTO is respectfully requested to make the attached document part of the record in the present application.

CONCLUSION

Should there be any outstanding matters that need to be resolved in the present application, the Examiner is respectfully requested to contact David R. Murphy (Reg. No. 22,751) at the telephone number below, to conduct an interview in an effort to expedite prosecution in connection with the present application.

If necessary, the Commissioner is hereby authorized in this, concurrent, and future replies, to charge payment or credit any overpayment to Deposit Account No. 02-2448 for any additional fees required under 37 C.F.R. §§ 1.16 or 1.17; particularly, extension of time fees.

Respectfully submitted,

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JWB/DRM/enm 1422-0416PUS2

PATENT 1422-0416PUS2

IN THE UNITED STATES PATENT & TRADEMARK OFFICE

In Re Application of

Yutaka KANAMARU et al.

Group Art Unit:

Serial No.: 10/815,790

Filed: April 2, 2004

Examiner:

For: TONER FOR DEVELOPMENT OF ELECTROSTATIC LATENT

IMAGES

DECLARATION UNDER 37 C.F.R. 1.132

HONORABLE COMMISSIONER OF PATENTS & TRADEMARKS WASHINGTON, D.C. 20231

Sir:

- I, Yutaka KANAMARU, residing in Wakayama-shi, Wakayama-ken, Japan, hereby declares and states as follows:
- 1. That I am one of the co-inventors of U.S. Application Serial No. 10/815,790 filed on April 2, 2004, entitled TONER FOR DEVELOPMENT OF ELECTROSTATIC LATENT IMAGES. I am thoroughly familiar with the contents of said Application, its prosecution before the United States Patent and Trademark Office and the references cited therein.
- 2. That I am a graduate of Graduate School of Osaka City University, Faculty of Applied Chemistry in the year 1985, majoring in organic chemistry.
- 3. That I have been employed in Kao Corporation in the year 1985 and have been assigned to the Research Laboratories.

- 4. That I have been involved in the research and development of toner since 1987.
- 5. That the following experiments were conducted by myself or under my direct supervision and control in order to verify that the present invention exhibits superior effects over Uchida et al. (Uchida), USP 4,863,824.

EXPERIMENTS

Preparation of Polyester

Resins 2-2c and 2-3 used in Example 5 of Uchida were reproduced by the following methods.

Starting materials the recipes of which are shown in Table A were charged into a four-necked flask (capacity, 2 l) equipped with a thermometer, a stainless steel stirrer, a nitrogen introducing glass pipe and a dropping condenser. The flask was set in a mantle heater and reaction was carried out with stirring at 200°C in a nitrogen atmosphere. The progress of the reaction was monitored by an acid value measurement. At the time when a predetermined acid value was attained, the reaction was quenched and the reaction product was cooled to room temperature to yield polyester samples in the form of a pale yellow solid.

The characteristic values of the polyester samples are noted in Table B.

Table A

Polyester No.	Alcohol component		Acid component		
	Polyoxypropylene (2.2)-2,2-bis (4-hydroxyphenyl) propane	Trimethylol- propane	Terephthalic Acid	Isododecenyl succinic acid	
2-2c	602g (1.75mol)	25.0g (0.19mol)	232g (1.40mol)	172g (0.65mol)	
2-3	447g (1.30mol)	67.0g (0.50mol)	232g (1.40mol)	172g (0.65mol)	

Table B

Polyester No.	Softening Point (°C)	Glass Transition Point (°C)	Chloroform Insolubles (wt %)
2-2c	143	68	14.3
2-3	102	61	0

Preparation of Toner

60 parts by weight of Polyester 2-2c, 40 parts by weight of Polyester 2-3, wax shown in Table C and 10 parts by weight of carbon black "Mogul L" (product of Cabot Corporation) were preliminarily blended and subjected to a standard process consisting of melting, kneading, cooling, grinding and classification. As a result, untreated toners having an average particle size of 10 μm were obtained.

The amount 0.3 parts by weight of a hydrophobic silica "H-2000" (manufactured by Wacker Chemical Co.) was blended with 100 parts by weight of each of the resulting untreated toners by using a Henschel mixer to give each of the toners.

Evaluation of Toner

Test Example I

A developer was prepared by blending 32 parts by weight of each of the toners with 768 parts by weight of silicone-coated ferrite carrier (average particle size: 90 µm).

The same procedures as in Test Example 1 of the present invention were carried out to determine the lowest fixing temperature and the hot-offset generating temperature, except that the copy machine was changed from a modified apparatus of "SF9800" (manufactured by Sharp Corporation) to a modified apparatus of "AR-505" (manufactured by Sharp Corporation), and that the reflective densitometer was changed from RD-915 (manufactured by Macbeth Process Measurements Co.) to "SPM-50" (manufactured by GRETAG). Different apparatuses from those described in the present specification were used in the test because the manufactures and sales of the apparatuses were terminated.

Specifically, each of the developers prepared as described above was loaded on a copy machine [a modified apparatus of "AR-505" (manufactured by Sharp Corporation) which was equipped with an organic photoconductor and a fixing roller having a rotational speed of 250 mm/sec, set to have variable heat roller temperatures, and a fixing unit having no oil applying device]. By sequentially increasing the fixing roller temperature from 90°C to 240°C, the formed images were developed to determine the lowest fixing temperature and the hot offset generating temperature by the following methods. The results are shown in Table C.

(1) Lowest Fixing Temperature

The lowest fixing temperature used herein referred to the temperature of the fixing roller at which the fixing ratio of the toner exceeded 70%. This fixing ratio of the toner was determined by placing a load of 500 g on a sand-rubber eraser (LION No. 502) having a bottom area of 15 mm × 7.5 mm on a fixed toner image obtained in the fixing device, moving the loaded eraser on the image backward and forward five times, measuring the optical reflective density of the image before or after the eraser treatment with a reflective densitometer "SPM-50" manufactured by GRETAG, and then calculating the fixing ratio by the following equation.

Fixing Ratio
$$= \frac{\text{Optical density}}{\text{Optical density}} \times 100$$
before eraser treatment

(2) Hot-Offset Generating Temperature

Fixed images were developed at each temperature, and subsequently blank image-transfer paper was conveyed through the fixing roller under the same conditions as above. The "hot offset generating temperature" is referred to a temperature of the fixing roller at which toner dusts were initially generated on the blank paper.

Test Example II

The same procedures as those described in Test Example 2 of the present invention were carried out. Specifically, a 100 ml glass bottle was charged with 10 g of each toner, and the blocking resistance was evaluated after the toners were

allowed to stand under the conditions of 50°C temperature and 26% relative humidity for two weeks in accordance with the following evaluation criteria:

- O: Completely no blocking was observed.
- ×: Toner was in a hard caking state.

The results are shown in Table C.

Test Example III

The same procedures as those described in the portions beginning at page 24, bottom line to page 25, line 8 of the present specification were carried out except that the following simplified version of the test method was carried out in order to complete the test within the given time frame. Specifically, a 100 ml glass bottle was charged with 1.6g of a toner and 38.4g of a silicone-coated ferrite carrier (average particle size: $90~\mu m$), the resulting mixture was mixed for 12 hours with a turbuler mixer at a rotational speed of 90~r/min. Thereafter, the toner was aspirated from the resulting mixture using a 400-mesh sieve having a sieve-opening of 34 μm , to leave only the carrier. The carbon content of the resulting carrier is determined using a carbon analyzer "EMIA-110" (commercially available from HORIBA, LTD.). The carbon content of the carrier was evaluated as durability. The results are shown in Table C.

In the two-component developer for electrophotography, the toner gradually stains the carrier surface during a long-term use, so that the triboelectric chargeability of the carrier is worsened, whereby charging failure of the toner is increased, which in turn ends up a background fogging on the fixed image.

Generally, this state is referred to as a life of the developer. The evaluation of the durability of the toner can be made by carrying out a life test for a developer by changing toners while using the same carrier in an actually used developer. However, in the declaration, as a simplified test, the life is evaluated by the degree of toner staining on the carrier after vigorously agitating a developer for a long period of time.

Usually, in toners having poorer dispersibility of the internal additives such as a wax, the internal additives are exposed to surfaces of a finely pulverized toner. The internal additives are detached from the surface upon the agitation in the developer device, so that the exposed internal additives are likely to be migrated from the toner to the carrier, whereby lowering the triboelectric charges of the carrier, thereby making the life of the developer shorter.

The lower the durability of the toner, the more the internal additive is likely to be adhered to the carrier surface, whereby the carbon content of the carrier is increased. In other words, the higher the carbon content of the carrier after the agitation, the poorer the durability of the toner.

Table C

	Wax 1)	Amount (parts by weight)	Melting Point (°C)	Lowest Fixing Temp. (°C)	Hot-Offset Generating Temp. ²⁾ (°C)	Blocking Resistance	Durability (%)
Toner 1				128	200	0	0.05
Toner 2	Polypropylene Wax	5	135,144	122	240<	0	0.25
Toner 3	Carnauba Wax	1	84	102	240<	\circ	0.07
Toner 4	Carnauba Wax	5	84	98	240<	0	0.08
Toner 5	Carnauba Wax	7	84	96	240<	×	0.18
Toner 6	Rice Wax	5	78	100	240<	0	0.09
Toner 7	Fischer- Tropsch Wax	5	72	103	240<	×	0.32

¹⁾ Polypropylene Wax:

Carnauba Wax:

Fischer-Tropsch Wax:

[&]quot;Viscol 660P" [manufactured by Sanyo Chemical Industries, Ltd., melting points: 135°C, 144°C (2 peaks detected by DSC)]

[&]quot;Carnauba Wax No. 1" [manufactured by K.K. Kato Yoko, melting point: 84°C] Rice Wax:

[&]quot;M-90" [manufactured by K.K. Serarika-Noda, melting point: 78°C]

[&]quot;FT-0070" [manufactured by Nippon Seiro Co., Ltd, melting point: 72°C]

^{2) &}quot;240<" means that no offset is generated at 240°C.

RESULTS AND DISCUSSION

It is found from the above results that Toners 3, 4, and 6 each comprises a given amount of an ester wax having a low melting point, all of which give excellent results in their performances.

On the other hand, Toner 1 not containing an ester wax is unsatisfactory in low-temperature fixing ability and offset resistance, and Toner 2 containing a high-melting point wax, which is the closest example to Toner 5 of Uchida, is unsatisfactory in low-temperature fixing ability and durability.

Toner 5 having an exceedingly high content of the low-melting point wax is unsatisfactory in blocking resistance and durability.

Furthermore, Toner 7 containing a wax other than the ester wax is unsatisfactory in blocking resistance and durability even though the wax was a low-melting point wax. The reason therefor is presumably due to the lowering of the compatibility of the resin binder with the wax, as compared to that with the ester wax.

Therefore, it is clear that by the adjustment of the melting point of the wax but also the kind and the content of the wax, the obtainment of the excellent results for all of low-temperature fixing ability, offset resistance, the blocking resistance and the durability is a surprising effect which would not have been expected by one of ordinary skill in the art simply from the disclosure of Uchida.

- 6. The undersigned petitioner declares further that all statements made herein of his own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of this application or any patent issuing thereon.
 - 7. Further declarant saith not.

Yutaka KANAMARU

April 28, 2004

Date